

Determination of Contours of Flooded Areas Due to Possible Accident of Zhinvali (Georgia) Earth Dam and Calculation of the Hydrodynamic Parameters of a Destructive Wave at a Dam

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Abstract. Using theoretical and field studies, computer software programs (VOLNA-4, and MIKE-21,) and GIS technology, and taking into account the possible accident (destruction) of the Earth Dam with a height of 102 meters, the contours of the riverbed of flooded territories in riverbeds for rivers Aragvi and Mtkvari have been defined in the given article considering the configuration of the water-catchment basins of rivers.

By means of basic differential equations of hydraulics, geometrical dimensions of Zhinvali Earth Dam, hydrological basic parameters of the reservoir, and computer software, the basic hydrodynamic parameters of the destructive wave at the Zhinvali Earth Dam are calculated taking into account the time of flow movement.

Keywords: earth dam, accident, flood, risk, flooded territories.

1. Introduction

The reason for the disruption of hydraulic facilities, including Zhinvali Earth Dam (Georgia) may be natural calamities (earthquake, storm, mudflow, etc.), technogenic factors (corrosion and collapse of the building structures, violation of water intake regimes, etc.), as well as sabotage and terroristic acts and use of arms destructing dams during the war.

In case of disruption of a hazardous hydrodynamic plant, a 102-meter-high Zhinvali Earth Dam (Fig. 1) in our case, breakdown tsunami-type waves are formed potentially. The strength of the waves depends on the amount of water and wave velocity. Therefore, the hydrodynamic objects with great amount of water in their reservoirs and with a great difference between the heights of their head and tail races (high head), are hazardous in this respect.

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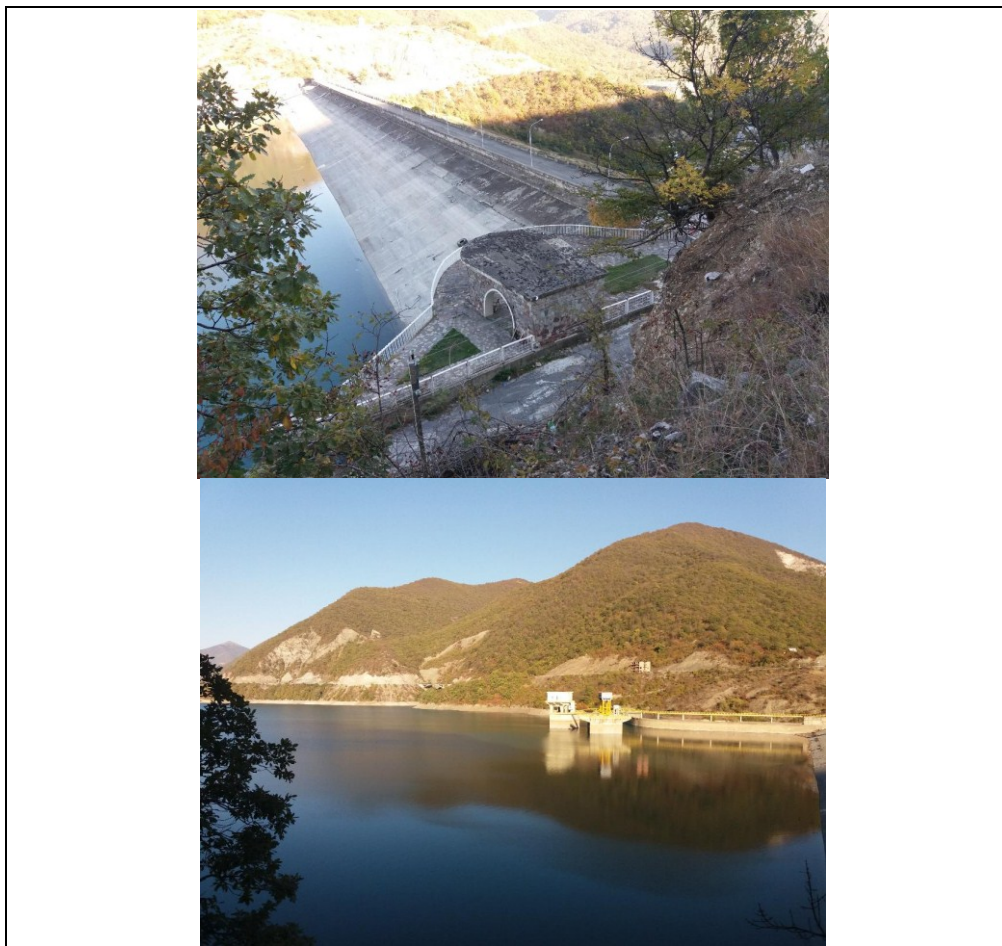


Fig. 1. General view of Zhinvali Earth Dam and reservoir

A breakdown wave and great water mass can overwhelm everything on their way: buildings, premises and agricultural plots, and may result in victims and great material losses [2].

The main function of Zhinvali Earth Dam is to protect the environment, economic objects and human life from the floods formed in the bed of the Aragvi River. However, in terms of incorrect exploitation of the dam and under the action of extreme natural phenomena (earthquake, catastrophic floods, etc.), Zhinvali Earth Dam itself may be a reason for a big catastrophe.

Following the category of a safety risk of a hydraulic facility (technological, environmental or social) and by considering a safety declaration of a facility owner, the terms of a dam operation must be observed by means of a safe operation and checks of the terms of no-failure operation of the plant units and all auxiliary facilities, buildings and equipment.

By considering the EU Directive on the assessment and management of flood risks in Georgia (January 1, 2012, <http://www.slovakaid.sk/>), a harmonization [2] and implementation mechanism must be incorporated in the legislation of the country what implies as follows:

- Developing a roadmap for harmonization and implementation of the EU Directive on the assessment and management of flood risks in the legislation of Georgia;

- Developing a draft responsibility and actions Directive in the field of flood forecast and early warning for relevant ministries, what means:
 - The development of methodologies in the area of the flood risks and hydrological monitoring;
 - Developing the methodologies to draft the area of floods risks;
 - Developing the map of the zones of flood risks in the basins in the GIS system for the whole country;
 - Introducing modern hydrological models to predict floods;
 - Providing automated hydrological posts in the water catch basins of the rivers;
 - Training young experts in flood prediction issues, etc.

2. THE METHODOLOGY TO CALCULATE HYDRODYNAMIC PARAMETERS OF TSUNAMI-LIKE WAVE

With the aim to provide a computer imitation of possible technogenic catastrophes of Zhinvali Earth Dam, modified software VOLNA-4 and MIKE-4 algorithms were used and field studies of Zhinvali Dam were accomplished on February 10-27 (Fig. 2 and 3) what allows calculating the hydrodynamic parameters of the dam breakthrough wave in case of possible dam destruction, in particular: wave velocity, covered distance and more importantly, the sizes of the flooded area in relation to time.

The initial data were divided into two parts by us: the first is the permanent values and another is variable values. Permanent values consider the parameters not dependant on some or other condition; as for the variable values, they depend on flood, degree of dam destruction, etc.

The construction height of Zhinvali Earth Dam is 102 m and its effective height (water flooding height) is 96 m. The dam width varies within 415 m; the capacity of Zhinvali water reservoir is 520 mln. m³, while the water surface area is 733 mln. m³ [4].

In our case, in case of destruction of Zhinvali Earth Dam, destructing tsunami-like waves are formed potentially. The strength of the waves depends on the amount and velocity of water. Therefore, the hydrodynamic objects with great amount of water in their reservoirs and with a great difference between the heights of their head and tail races (high head), are hazardous in this respect.

A breakdown wave and great water mass can overwhelm everything on their way: buildings, premises and agricultural plots, and may result in victims and great material damage.

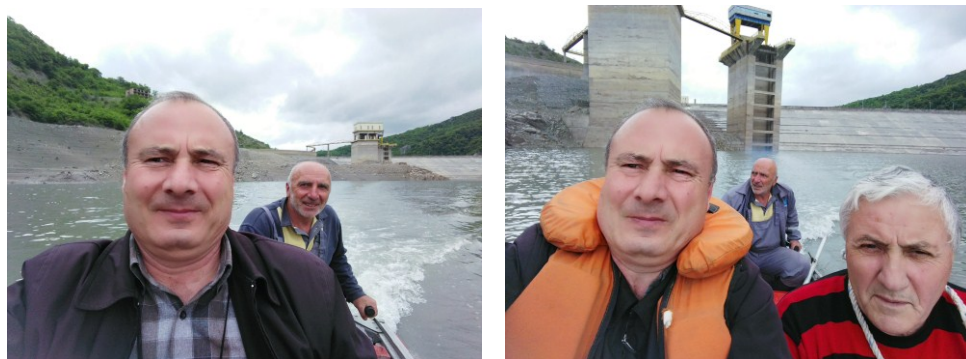


Fig. 2. Swimming on a motorboat in Zhinvali reservoir during the field studies



Fig. 3. General view of colloid and sandy material deposited in Zhinvali reservoir

Figure 4 shows a longitudinal profile of a tsunami-type wave formed in case of destruction of Zhinvali Earth Dam.

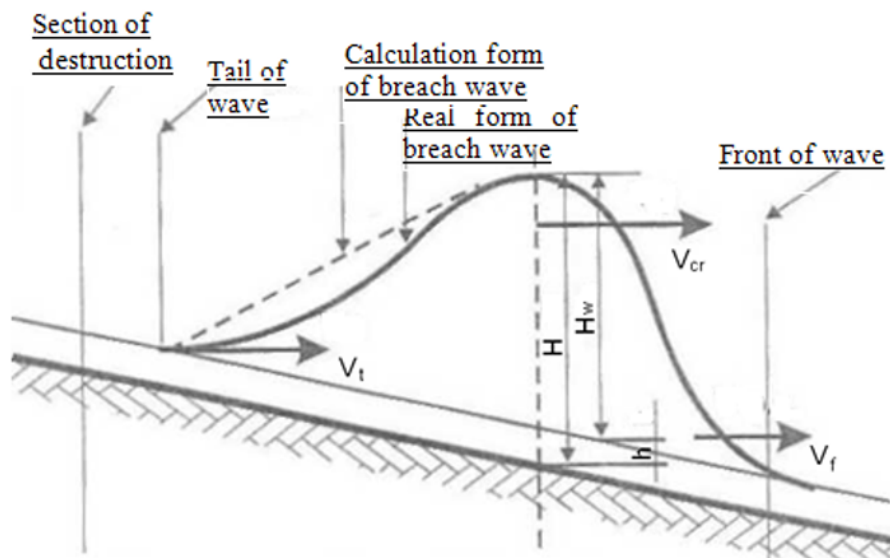


Fig. 4. Longitudinal profile of a tsunami-like wave

The volume of water in the reservoir (W_0) was calculated with the following dependence [2,5,5,10]:

$$W = \frac{H_B S_B}{3} \quad (\text{mln. m}^3) \quad (1)$$

Where H_B is the water depth at the height of normal dam flooding (m); S_B is the area of the water surface in the reservoir (mln. m³);

The width of river is taken from the topographic maps. As for the number of points, it must not exceed 3 points on the each side of the river axis, i.e. total of 6 points, and must cover the whole water catch area. In order to calculate the area of the flooded territory, the number of sections from the dam must not exceed 8, with the distance between them to be plotted on a topographic map in advance.

The wave velocity (V) during the flood is calculated by the following formula in the tailrace of the facility [10]:

$$V = V_0 (H_1 / H_0)^{2/3}, \quad (\text{m/sec}) \quad (2)$$

The degree of the dam destruction (E_p) was established with the following expression [64]:

$$E_p = \frac{F_B}{F_0}, \quad (3)$$

Where F_B is the area of the bank breach (m^2); F_0 is the surface area (m^2).

Besides the above-mentioned, the algorithm considers: the height of the river bank edge (m), number of sections along the river, distance between the sections (km), width of the riverbed (m), water current velocity in the riverbed (m/sec); width of the bed of the Nogha River (m), values of the river levels (m), etc.

Zhinvali water reservoir, with its Dam representing a structure with a fill clay is located in village Zhinvali, Dusheti Region. The construction height of the Dam is 102 m and its effective height (water flooding height) is 96 m. The Dam width varies within 415 m; the capacity of Zhinvali water reservoir is 520 mln. m^3 , while the water surface area is 733 mln. m^3 (see Fig.5).



Fig. 5. View of Zhinvali Earth Dam from the tailrace

3. IDENTIFYING THE CONTOURS OF THE AREAS FLOODED AS A RESULT OF A POSSIBLE ACCIDENT OF ZHINVALI EARTH DAM

The number of sections from the Aragvi River to the Mtkvari River taken to predict the catastrophe of Zhinvali dam is 8 (Fig. 6).

The sections were taken in the following settled areas located at different distances from the dam, in particular, 1) village Misaktsieli – 30,0 km; 2) Avchala settlement - 35,0 km; 3) Dighomi (Shalikashvili) Bridge - 44,5 km; 4) Tamar Mepe (Chelyuskinites) Bridge - 48,0 km; 5) Ortachala Bridge - 54,2 km; 6) new settlement of Rustavi - 74,0 km; 7) center of Rustavi - 77,0 km; and 8) end point of Rustavi - 80,0 km.

By using the theoretical and field studies, computer software (VOLNA – 4 and MIKE-21) and GIS technology [2-8,10,12], by considering a possible accident of a 102-meter-high Zhinvali Earthen Dam (Georgia) with 0.75 degree, the contours of the beds of the flooded areas in the Aragvi and Mtkvari Riverbeds were identified by considering the configuration of the water catch basins of the Rivers. The results of the calculation are given Table #1.

Detailed data about Zhinvali Dam are given in the Tables below (Tables 2 and 3) and the sizes of the flooded areas in the riverbed and in the adjacent areas are given in Figures 7-15.

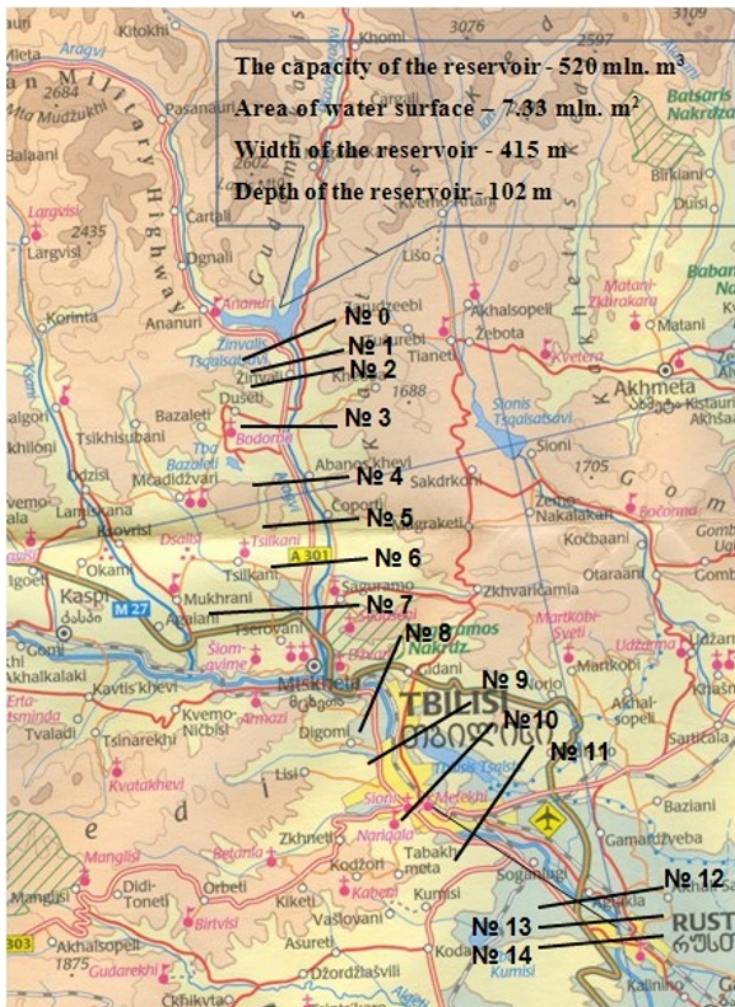


Fig. 6. Plan of location of design sections

Table 1. Description: Zhinvali Dam (With Destruction Degree $E_3 = 0,75$)
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Initial data of the hydrological system :	Unit of meas.	Number
1. Water reservoir capacity at standard flooding level (SFL)	mln. m ³	520
2. Reservoir depth at SFL	m	96
3. Water surface area at SFL	mln. m ³	7,33
4. dam width at SFL	m	415
5. River depth in the Dam tailrace	m	1
6. River width in the Dam tailrace	m	25
7. River velocity in Dam tailrace	m/sec	1
8. Reservoir depth at the moment of the dam accident	m	96
9. Dam destruction degree	m	0,75
10. Height of the riverbed bank breach	m	24
11. Water standard flooding level in the reservoir	m	816
12. Number of lateral profiles in the riverbed	pcs.	8

Table 2. Calculated numerical values

Cross sections	Unit of meas.	Secti on #1	Secti on #2	Secti on #3	Secti on #4	Secti on #5	Secti on #6	Secti on #7	Secti on #8
1	2	3	4	5	6	7	8	9	10
Distance of $a^{i^{th}}$ section from the Dam	km	30	35	44,5	48	54,2	74	77	80
Specific current:									
Water flooding level	m	480	425	398	393	375	327	322,7	313
Depth	m	1	3	2	2	1	2	1	1
Width	m	70	60	80	82	80	150	100	93
Current velocity	m/sec	1	1	1	1	1	1	1	1
Left bank									
Height of the river bank breach	m	7	2	3	5	4	2,5	3	0,5
Width of the Nogha River bed	m	50	10	50	20	20	5	5	40
Level #1	m	490	435	402,5	400	383	330	327,5	315
Distance from the river axis to level #1	m	137	50	440	71	180	100	60	225
Level #2	m	520	440	405	405	385	340	330	320
Distance from the river axis to level #2	m	687	70	670	371	280	125	1310	1295
Level #3	m	680	490	410	415	388	350	332,5	322,5
Distance from the river axis to level #3	m	2437	340	970	800	720	265	1610	1345
Right bank									
Height of the river bank breach	m	15	8	3	5	4	1	1	5
Width of the Nogha River bed	m	30	25	50	20	100	300	300	50
Level #1	m	520	435	402,5	410	380	330	325	340
Distance from the river axis to level #1	m	912	60	840	90	510	525	750	440
Level #2	m	600	445	405	415	385	340	337,5	350
Distance from the river axis to level #2	m	1137	70	1680	200	660	600	900	570
Level #3	m	680	490	410	425	395	343	345	400
Distance from the river axis to level #3	m	1637	540	2000	230	940	1300	1650	840

Table 3. Hydrological values of the flooded area

Dam destruction parameters	Unit of meas.	Section #0	Section #1	Section #2	Section #3	Section #4	Section #5	Section #6	Section #7	Section #8
Distance of the section from the hydrological station	km	0	30	35	44,5	48	54,2	74	77	80
Water peak discharge in the section	thous. m ³ /sec	137	24,4	21,9	18,12	17,2	15,59	12,32	11,84	11,5
Time:										
Of wave front descending	min	0	47,1	57,8	76,9	90,9	108,5	175,5	186,7	201
Of wave descending	min	0	80,2	99,1	143,4	158	180,7	288,7	301,9	314,8
Wave tail descending	min	149	649	732	890,4	949	1052	1382	1432	1482
Of flooding	min	149	602	674	813,5	858	943,6	1207	1245	1281
Maximum flow velocity	m/sec	18,7	11,2	14,1	5,03	9,53	6,77	6,86	4,91	5,26
Wave height	m	56,6	18,6	29,7	6,15	14,8	8,29	7,88	4,88	5,41
Maximum flooding depth	m	57,6	19,6	32,7	8,15	16,8	9,29	9,88	5,88	6,41
Maximum flooding level	m	778	499	455	404,2	408	383,3	334,9	327,6	318,4
Maximum flow height:										
On the left bank of the river	m	152	294	862	591,6	614	211,7	112,2	97,83	955,8
On the right bank of the river	m	152	185	524	1394	84,8	608,8	561,6	780,9	103

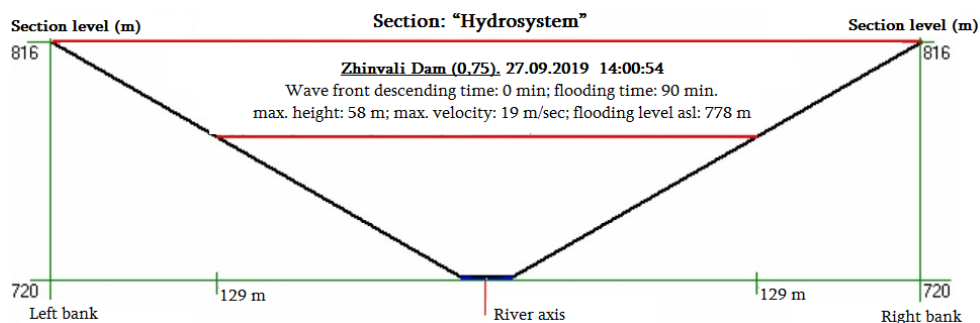


Fig. 7. Section of Hydrosystem

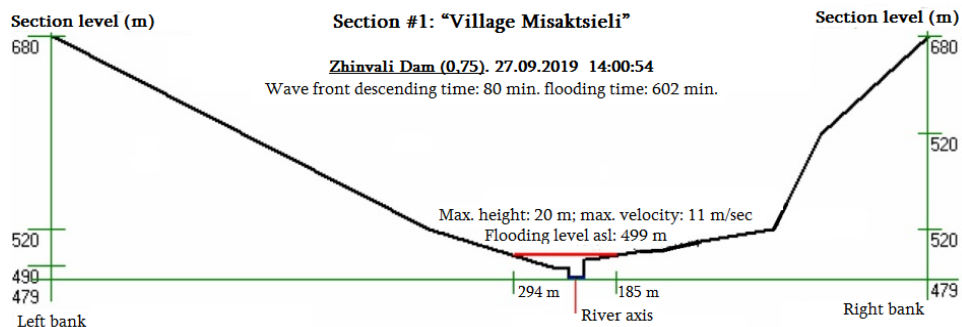


Fig. 8. Section #1, Village Micaktsieli

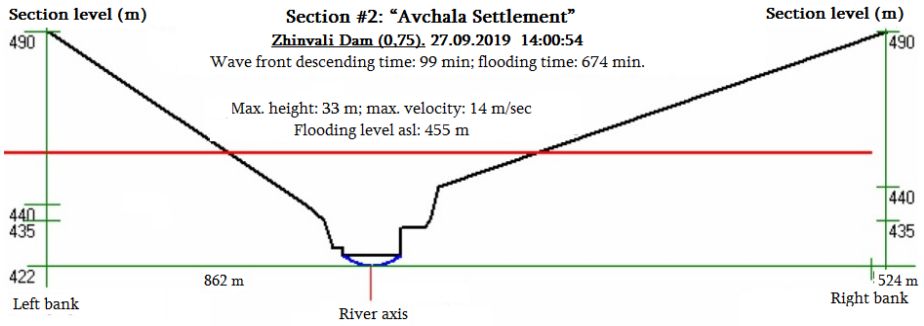


Fig. 9. Section #2, Village Avchala Settlement

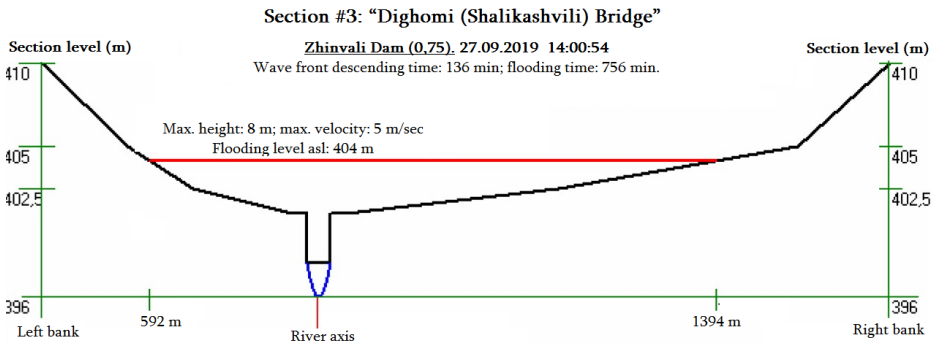


Fig. 10. Section #3, Dighomi (Shalikashvili) Bridge

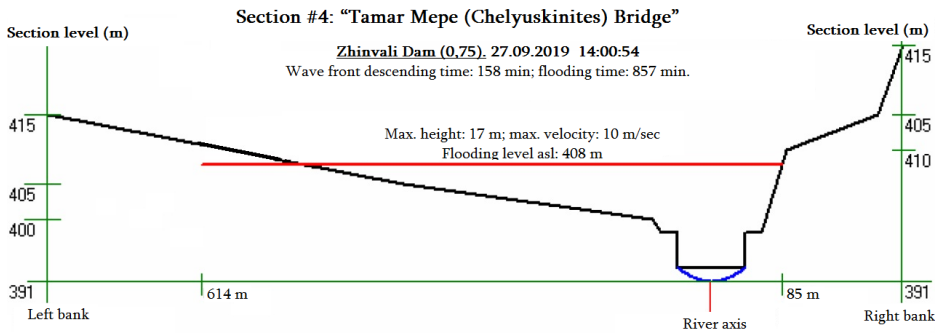


Fig. 11. Section #4, Tamar Mepe (Chelyuskintses) Bridge

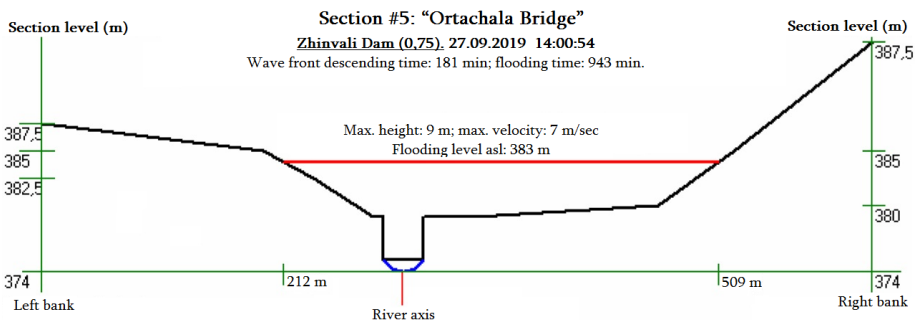


Fig. 12. Section #5, Tamar Ortachala Bridge

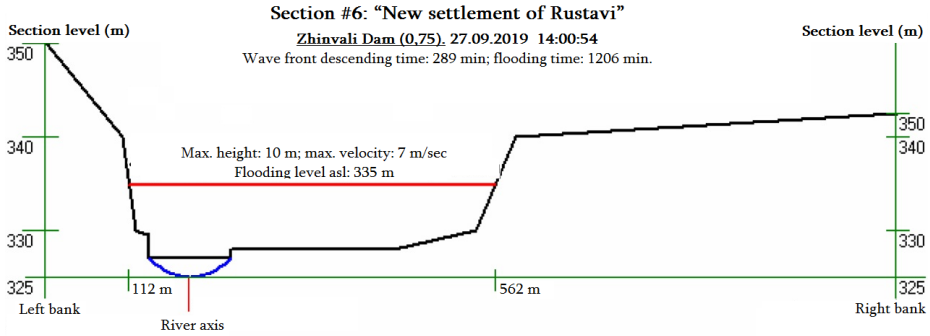


Fig. 13. Section #6, New settlement of Rustavi

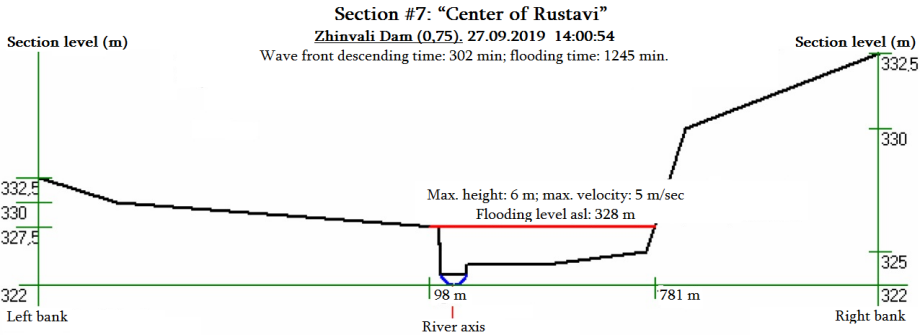


Fig. 14. Section #7, Center of Rustavi

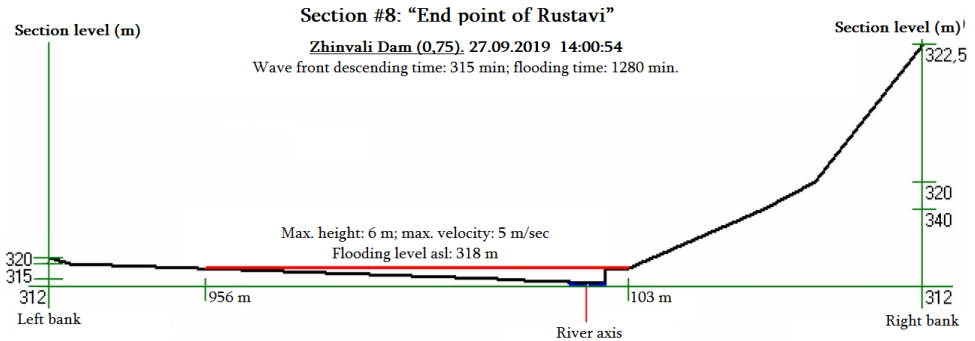


Fig. 15. Section #8, End point of Rustavi

As for the hydrodynamic data of a tsunami-type wave formed following the accident with 0.75 destruction degree of Zhinvali Dam by considering the time factor, the geometrical data of the flooded area are given in Table #4.

Table 4. Geometric data of the flooded area

#	Section	Tsunami wave motion time (min)	Width of the flooded area from the center of symmetry of the riverbed (m)		Height of tsunami wave (m)	Velocity of tsunami wave (m/sec)
			Right	Left		
1	Village Misaktsieli	47,1	322	319	21	11
2	Avchala settlement	57,74	The canyon gets flooded on both sides			
3	Dighomi (Shalikashvili) Bridge	76,34	1603	649	9	5
4	Tamar Mepe (Chelyuskinites) Bridge	90,1	715	88	18	10
5	Ortachala Bridge	107,0	629	239	10	7
6	New settlement of Rustavi	172,6	570	115	11	7
7	Center of Rustavi	183,3	786	293	6	5
8	End point of Rustavi	197,3	110	1055	7	5

Thus, based on the field, theoretical and experimental studies, the principal hydrodynamic properties of Tsunami wave formed as a result of possible destruction of Zhinvali Earth Dam were identified by considering the relevant time factor and the geometry of the flooded area was determined as well.

The risk zones of the flooded areas were specified and the norms of behavior for the population in the state of emergency were developed [2,9].

4. Conclusions

Under the financial support of Grant Project # FR17_615 “Assessment of safety risks of vulnerable infrastructure during the formation of expected catastrophes”, based on the complex studies accomplished during the field scientific expeditions for Zhinvali Earth Dam in 2019-2020, we may draw the following conclusions:

1. As a result of the studies accomplished in Zhinvali reservoir, the statistical material was processed, which allows specifying the volume of the solid drift deposited in the headrace of the Dam and minimum useful water capacity;
2. The samples of colloid fraction were taken from the reservoir area and a chemical analysis of the suspension was provided with the aim to use it for commercial purposes;
3. Based on the scientific studies in the tail and head races of Zhinvali Earth Dam, a longitudinal profile of a tsunami-type wave formed as a result of the possible dam destruction was determined by calculating relevant hydrodynamic parameters;
4. For the case of a 0,75% destruction degree of 102-meter-high Zhinvali Earth Dam, by using a mathematical model (VOLNA – 4 and MIKE-21) and GIS-technology, the contours of the riverbed of flooded territories in riverbeds for rivers Aragvi and Mtkvari have been defined by considering the configuration of the water catch basins of the rivers.
5. Based on the obtained data, the risk zones of the flooded areas were specified and the norms of behavior for the population in the state of emergency were developed.

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