

Graphical-analytical method for constructing load characteristics

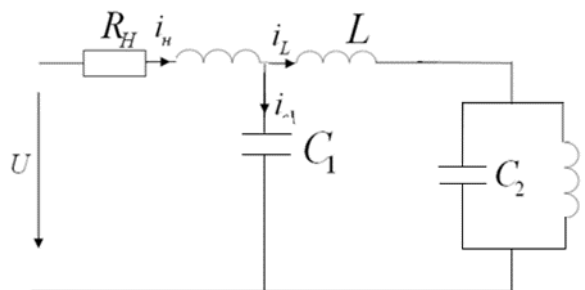
A N Rasulov¹, M R Ruzinazarov¹, N Toirova¹, Alibekova T Sh²

¹ Tashkent State Technical University named after Islam Karimov, 100095, Uzbekistan, Tashkent, University St. 2A

² Karakalpak State University, 230100, Uzbekistan, Nukus, Ch. Abdirov St.1

Abstract. The article discusses a graphical-analytical method for constructing the load characteristics of a three-element resonant circuit in the current stabilization mode. The current stabilization mode is observed when compensating the negative section of the S-shaped characteristics of the parallel resonant circuit of the connected sequence with a linear inductance and with a linear capacitor characteristic. The equation of the load mode in a dimensionless form represents the equation of an ellipse, which makes it possible to construct the necessary characteristics of a three-element resonant circuit for various types of load.

In engineering practice, various graphical methods for analyzing the operation of ferromagnetic devices have been applied. A graphical method is proposed for calculating the equivalent circuit of a three-element resonant circuit proposed in Fig. 1 in the current stabilization mode for a complex load.



In this case, the known current-voltage characteristic of the device for the unloaded mode and the currents of the branches of the circuit is assumed to be sinusoidal. [1-8] For the current stabilization mode with active-inductive load, the following equation is valid:

$$u = L_u \frac{di_c}{dt} + i_c R_H + u_c \quad (1)$$

For active-capacitive load

$$u = \frac{1}{C} \int i_c dt + i_c R_H + u_c \quad (2)$$

here: L_H , C , R_c , respectively, inductance, capacitance and active load resistance;

i_c - stabilization current;

u_c -voltage at the terminals of the three-element resonant circuit;

u -mains voltage;

$$\text{Accept } i_c = I_{cm} \sin \omega t, \quad u_c = U_{cm} \cos \omega t \quad ; \\ u = U_m \cos(\omega t + \psi)$$

Such an assumption is possible if the losses in the circuit of the circuit are neglected and provided that the circuit of the device operates in a capacitive mode. After some transformations and introduction of normalized values from (1) we get:

$$y_m^2 = (\gamma Z_m - y_{cm})^2 + \delta^2 \beta_1^2 Z_m^2, \quad (3)$$

Where

$$\gamma = \frac{L_H}{L}; \quad \delta = \omega C_1 R_H; \quad \beta_1 = \frac{1}{\omega^2 L C_1}; \quad y_{cm} = \frac{u_{cm}}{U_\delta} \\ ; Z_m = \frac{I_m}{i_\delta}; y_m = \frac{u_m}{U_\delta}.$$

For the case of active-capacitive load

$$y_m^2 = (\gamma_c Z_m + y_{cm})^2 + \delta^2 \beta_1 Z_m^2 \quad (4)$$

$$\text{Here } \gamma_c = \frac{1}{\omega^2 L C_H}$$

From (3) and (5), respectively, for active-inductive and active-capacitive loads we get:

$$y_m^2 = (\delta^2 \beta_1^2 + \gamma^2) Z_m^2 + y_{cm}^2 - 2\gamma Z_m y_{cm}, \quad (5)$$

$$y_m^2 = (\delta^2 \beta_1^2 + \gamma_c^2) Z_m^2 + y_{cm}^2 + 2\gamma_c Z_m y_{cm}, \quad (6)$$

These dependencies are equations of second order curves representing ellipses. We bring these equations to canonical form by rotating the coordinate axes through some angle α . Old coordinates through new ones are determined by the following expressions: [9-14]

$$Z_m = Z'_m \cos \alpha - Y'_{cm} \sin \alpha$$

$$Y_m = Z'_m \sin \alpha - Y'_{cm} \cos \alpha$$

Here α is the angle of rotation of the axes.

Substituting these values in (5), we have:

$$AZ_m'^2 + 2BZ'_m Y'_{cm} + CY_{cm}'^2 = 0, \quad (7)$$

Where

$$A = (\delta^2 \beta_1^2 + \gamma^2) \cos^2 \alpha + \sin^2 \alpha - 2\gamma \sin \alpha \cos \alpha,$$

$$B = (\cos^2 \alpha + \sin^2 \alpha) - (\alpha^2 \beta_1^2 + \gamma - 1) \sin \alpha \cos \alpha = 0,$$

$$C = (\delta^2 \beta_1^2 + \gamma^2) \sin^2 \alpha + \cos^2 \alpha + 2\gamma \sin \alpha \cos \alpha = 0,$$

The choice of the angle α is made in such a way that the coefficient B becomes zero. This will allow obtaining an expression for the angle of rotation γ ($\cos^2 \alpha - \sin^2 \alpha - (\delta^2 \beta_1^2 + \gamma - 1) \sin \alpha \cos \alpha = 0$,

From where

$$\operatorname{tg} 2\alpha = \frac{2\gamma}{\delta^2 \beta_1^2 + \gamma - 1}$$

For active capacitive load

$$\operatorname{tg} 2\alpha = \frac{2\gamma_c}{\delta^2 \beta_1^2 + \gamma_c - 1}$$

Now we bring equation (7) to the form

$$AZ_m'^2 + CY_{cm}'^2 = Y_m'^2$$

Or

$$\frac{Z_m'^2}{\frac{Y_m'^2}{A}} + \frac{Y_{cm}'^2}{\frac{Y_m'^2}{C}} = 1 \quad (8)$$

Thus, the connection between Z_m and Y_{cm} for a fixed value of the load is determined by the equation of the ellipse (8) and the known current-voltage characteristic of the current stabilizer circuit. The graphical method allows you to visually analyze the load mode of the current stabilizer and build the necessary characteristics of the device. [15-21] For the case of active load, the canonical form of the ellipse equation is as follows:

$$\frac{Z_m^2}{\frac{Y_m^2}{\delta^2 \beta_1^2}} + \frac{Y_{cm}^2}{Y_m^2} = 1 \quad (9)$$

Using the known values of the semiaxes $\frac{Y_m}{\delta \beta}$ and Y_m plotted on the characteristics $Z_m = f(Y_{cm})$ of the stabilizer of the ellipse. The intersection points define the corresponding values and Z_m and Y_{cm} . Figures 2 and 3 show a graphical method for determining the quantities of interest for the case of active, active-inductive and active- capacitive characteristics. The constructed adjustment and external characteristics according to the graphical method [22-28]

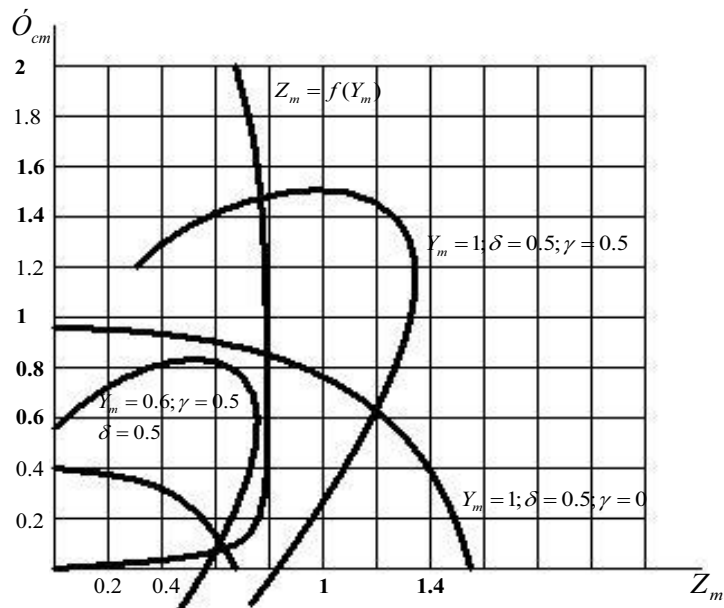
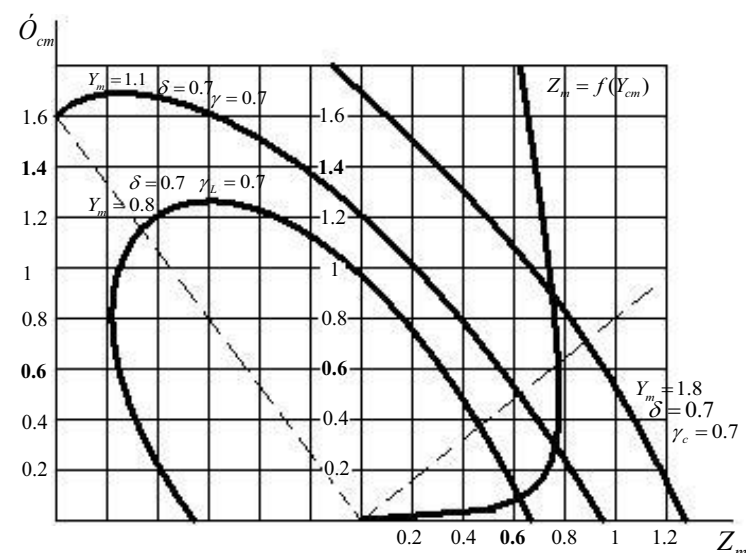


Figure: 2. Graphic method for determining Z_m, U_{cm}



Conclusions

1. Based on the analysis of the three-element resonant circuit, the possibilities of stabilizing the load current are revealed.
2. The relationship between the load current and the voltage of a parallel connected capacitor for a fixed load value is determined by the ellipse equation and the current-voltage characteristic of the current stabilizer circuit, which allows you to visually analyze the load mode and build the necessary characteristics.

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