# Axial Vibration Analysis of Thrust Support of Vertical Hydrogenerator Unit

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**Abstract**. Axial vibration is the main accident that affects the normal function of the vertical hydro-generator unit and endangers the use of the unit. There are many reasons for the axial vibration of the unit. This article only analyzes the mechanism of the axial vibration of the thrust bracket of the vertical unit caused by the connection of the thrust head and the mirror plate, and gives a real machine measurement example and treatment measures.

# 1 Preface

The lateral vibration of the guide bearing of the hydrogenerator unit has received enough attention, while the axial vibration of the thrust bracket has not attracted people's attention. Tests have shown that a small axial vibration amplitude is enough to damage the components of the unit and bring unstable factors to the operation of the unit.<sup>[1]</sup> Since the excitation of axial vibration comes from many aspects such as water flow, machinery, elevtromagnetics, etc. [2][3][4][5], it is difficult to determine the excitation parameters quantitatively, and the problem of axial vibration has not yet been satisfactorily resolved. This paper takes a real machine test of a vertical hydro-generator unit as an example, analyzes the mechanism of the axial vibration of the thrust support of the unit caused by the deformation of the insulating backing plate and the mirror plate, and proposes treatment measures, which provide some experience for the fault diagnosis of the unit.

# 2 Vibration mechanism analysis

The weight and water thrust of the rotating part of the hydro-generator set act on the thrust bearing through the mirror plate connected by the thrust head. The thrust bearing is composed of several sector-shaped tiles with a certain gap between the tiles (Figure 1). Due to the unevenness of the insulating backing plate and the unevenness of the joint surface between the thrust head and the mirror plate, there is a gap between the thrust head and the mirror plate. When the gap is transferred to the thrust pad, the gap becomes smaller due to extrusion, the thrust pad is unloaded. When it turns to the thrust pad gap, it becomes larger due to slack, and the thrust pad is loaded at this time. This kind of loading and unloading alternately becomes an alternating force, and this alternating force causes the unit to produceaxial vibration. When the unevenness of the insulating backing plate is two steps, it will form an axial vibration with a frequency of twice the speed.

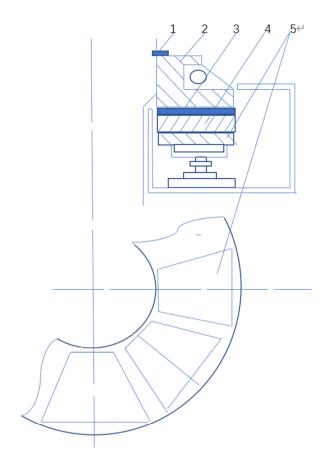
# 3 Vibration test of a vertical hydrogenerator unit

### 3.1 The source of the problem

A vertical shaft impact type turbine generator unit capacity 14000 KW, turbine type CJA575C-L-150/4  $\times$  11, the rotational speed of 600r / min, the thrust tile 8. After the extended overhaul of the unit, the start-up test found that the upper frame (thrust support) of the unit had a large axial vibration when it was above 45 Hz, and it was high-frequency vibration. After disassembling the machine to adjust the force of the thrust pad, the level of the mirror plate and the axis of the unit, restart the machine, and the problem still exists.

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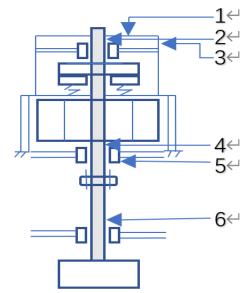
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1-Snap ring 2-Thrust head 3-Insuiation pad↔ 4-Mirror plate 5-Thrust pad↔ Figure 1 Schematic diagram of thrust head structure↔

#### 3.2 Test methods

The test method uses eddy current sensors to measure the swing of the shaft at the upper guide bearing, lower guide bearing and water guide bearing, the radial and axial vibration of the upper frame (thrust support), and the radial vibration of the lower frame(Figure 2). The computer automatically collects and analyzes each frequency and amplitude characteristics of measuring points.



1-Axial vibration of thrust bracket 2- Spindle swing at upper guide 3-Radial vibration of thrust bracket 4- Spindle swing at lower guide 5- Radial vibration of lower frame 6-Spindle swing at water guide

Figure 2. Location map of measuring points

	Table 1	Variable speed process test data			Unit: µm	
Rotating speed (rpm)	Thrust bracket radial vibration	Axial vibration of thrust bracket	Radial vibration of lower frame	Spindle swing at upper guide	Spindle swing at lower guide	Spindle swing at water guide
118.2	6.1	7.4	1.7	185.5	45	29.8
374.2	8.3	4.8	2.8	105.7	20	24.3
479.5	8.3	8.6	4.6	144.5	32.7	32.7
563.7	11.7	35.2	11.9	122.9	43.4	33
576.9	12.5	51.2	5.1	125.9	42.6	31
601.2	17.1	77.1	6.6	126.5	50.6	33.2
Ta	Unit: µm					
Working condition	Thrust bracket radial vibration	Axial vibration of thrust bracket	Radial vibration of lower frame	Spindle swing at upper guide	Spindle swing at lower guide	Spindle swing at water guide
Idling	18.4	86	6	122.5	53.7	33.7
25%ur	19.1	93.9	7	111.9	52.9	34.6
50%ur	18.7	94.3	6.1	115.1	50.6	34
75%ur	16.2	93.5	4	122.4	49.8	33.5
100%ur	14.7	88.4	6.9	119.7	49.2	33.6

## 3.3 Test Results

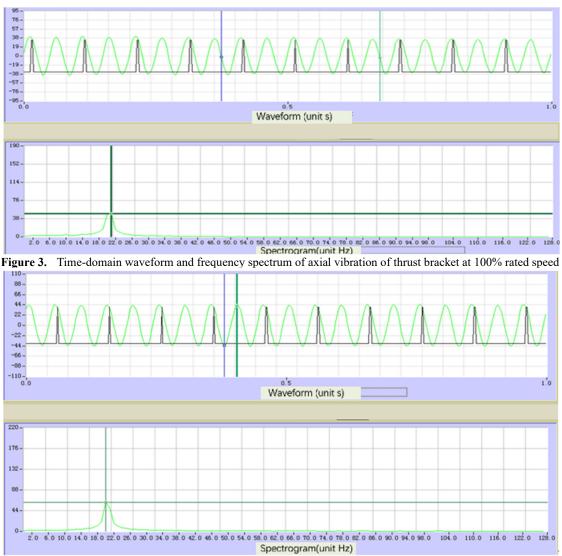


Figure 3 and Figure 4 show that the axial vibration frequency of the thrust bracket is 2 times the frequency of the unit in the idling and no-load conditions.

#### 3.4 Analysis of test results and inspection

Experimental data and by waveform analysis, and exclude the pressure fluctuation generator axis adjusting unit caused by poor axial vibration. The main factor that causes the thrust bracket to vibrate at 2 times the rotational speed is caused by the level of the mirror plate or the defect of the insulating backing plate.

The unit was in a random parking position, and the No. 4 and No. 8 thrust bearings were found to be loose after inspection. After tightening the loose thrust bearing, rotate the rotating part of the unit 90 degrees and then check the thrust bearing. The results show that No. 2, No. 3, No. 6, and No. 7 thrust bearings are loose.

Inspecting the insulating backing plate, it was found that the split surface of the insulating backing plate

Figure 4. Time-domain waveform and frequency spectrum of axial vibration of thrust support under no-load conditions became thinner, forming a shape with high sides on both sides and low in the middle, resulting in uneven joints between the mirror plate and the thrust head.

#### 3.5 Treatment measures

- (1) Replace with a new insulating backing plate.
- (2) The friction surface of the mirror plate is processed smoothly, and the wave of the mirror plate is completely eliminated.
- (3) Finely adjust the axis of the unit to reduce the swing value of the shaft at the upper guide bearing.

#### 3.6 Treatment effect

The axial vibration of the unit during operation is reduced (Table 3), and the vibration frequency is a composite frequency of 1 rpm, 2 rpm and 8 rpm (Figure 5), and the treatment effect has reached the expected purpose.

Table 3 Vibration test data							
Working condition	Thrust bracket radial vibration	Axial vibration of thrust bracket	Radial vibration of lower frame	Spindle swing at upper guide	Spindle swing at lower guide	Spindle swing at water guide	
150rpm	5.9	12.4	2.1	87.1	27.5	24.6	
300rpm	4.8	4.1	1.1	79.3	21.4	26.8	
450rpm	7.9	11	5	81.4	26.4	29.7	
600rpm	8.1	9	4.6	91.6	27.7	30.6	
No load	7.7	8.6	2.4	99.8	32.7	32.9	

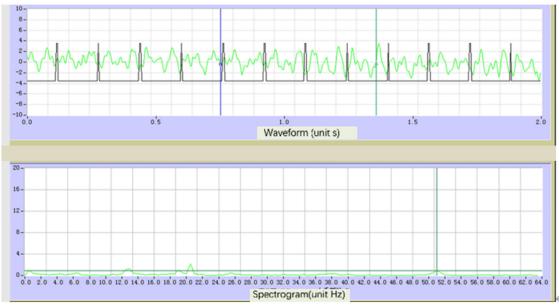


Figure 5. Time-domain waveform and frequency spectrum of axial vibration of thrust support under no-load conditions mechanical and electrical

## 4 Conclusion

There are many factors that cause the axial vibration of a vertical hydro-generator set, including mechanical factors, hydraulic factors and electromagnetic factors. This article only focuses on the thrust bracket axial direction of the vertical hydro-generator set due to the defects of the insulating backing plate and the mirror plate among the mechanical factors. A preliminary study on vibration was conducted. Due to the strong destructive force of axial vibration, a small vibration amplitude is enough to damage the components of the unit. Therefore, it is necessary to conduct in-depth research on the axial vibration of the vertical hydro-generator set caused by other factors.

This article provides some experience on the installation, maintenance and axial vibration fault diagnosis of vertical units.

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